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The 18th Korean Conference on Semiconductors

"Semiconductor beyond IT"

■ 일시 2011년 2월 16일(수) ~ 18일(금)
■ 장소 해비치 호텔 & 리조트 제주





관 하이닉스반도체, 한국반도체산업협회, 한국반도체연구조합

한국물리학회 반도체분과회, 한국재료학회, 대한전기학회 전기재료연구회, 대한전기학회 MEMS 연구회, 대한전자공학회 반도체재료 및 부품연구회, 대한전자공학회 SoC 설계연구회, 반도체설계교육센터(IDEC)

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M. RF Design 분과

Room D (크리스탈 D)

일 시:2월 17일(목) 10:40-12:00 세션명: [TD2] RF Circuit Blocks and Systems 좌 장: 이재성(고려대학교), 이강윤(건국대학교) TD2-1 10:40-11:00 A 140 GHz Divide-by-2 Inductive Feedback Injection Locked Frequency Divider in a 90nm CMOS Technology 저자: Hyogi Seo¹, Seungwoo Seo², Jongwon Yun¹, and Jae-Sung Rieh¹ 소속: ¹School of Electrical Engineering, Korea University, ²Agency for Defense Development TD2-2 11:00-11:20 A 9 Gb/s Optical Receiver Front-End with a Monolithically Integrated Avalanche Photodetector in 0.25 µm SiGe BiCMOS Technology 저자: J. S. Youn¹, M. J. Lee¹, K. Y. Park¹, H. Rücker², and W. Y. Choi¹ 소속: ¹Department of Electrical and Electronic Engineering, Yonsei University, ²IHP TD2-3 11:20-11:40 Design of Low-Jitter, Low-Power Clock Distribution Network with Inductive Peaking 저자: 한용수, 신보경, 김재하 소속: 서울대학교 공과대학 전기공학부 반도체공동연구소 0.046UI 지터와 ±1% 변조 비율을 갖는 1.5GHz 스프레드 스펙트럼 클 TD2-4 11:40-12:00 럭발생기 저자: 심창수, 변상진 소속: 동국대학교 전자전기공학부



2011년 2월 17일(목) 10:40-12:00

Room A 크리스탘 A	Room B 크리스탘 B	Room C 크리스탘 C	Room D 크리스탘 D	Room E 크리스탘 E	Room F 다이아몬드 A	Room G 사파이어	Room H B1 루비	Room I 다이아몬드 B	
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TD2

세션명 RF Circuit Blocks and Systems

좌 장 이재성(고려대학교), 이강윤(건국대학교)

TD2-1 10:40-11:00

A 140 GHz Divide-by-2 Inductive Feedback Injection Locked Frequency Divider in a 90nm CMOS Technology

Hyogi Seo¹, Seungwoo Seo², Jongwon Yun¹, and Jae-Sung Rieh¹ ¹School of Electrical Engineering, Korea University, ²Agency for Defense Development

In this work, a 140 GHz divide-by-2 injection locked frequency divider (ILFDs) employing inductive feedback has been developed in a commercial 90 nm Si RFCMOS technology. It was demonstrated that the injection locking is achieved with input power down to -9 dBm. At an input power of -3 dBm, the measured locking range was 0.75 GHz (143.7 - 144.45 GHz), consuming 10.2 mW DC power with a 1.8 V supply voltage. The fabricated chip size is 0.54 mm \times 0.69 mm including the DC and RF pads.

TD2-2 11:00-11:20

A 9 Gb/s Optical Receiver Front-End with a Monolithically Integrated Avalanche Photodetector in $0.25_{\mu m}$ SiGe BiCMOS Technology

J. S. Youn¹, M. J. Lee¹, K. Y. Park¹, H. Rücker², and W. Y. Choi¹ ¹Department of Electrical and Electronic Engineering, Yonsei University, ²IHP

An 850-nm optical receiver front-end having a monolithically integrated avalanche photodetector is realized for optical interconnect applications with standard $0.25_{\mu m}$ SiGe BiCMOS technology. Using fabricated optical receiver front-end, 9-Gb/s optical data are successfully transmitted with a bit-error ratio less than 10^{-9} at the incident optical power of -2 dBm.

A 9 Gb/s Optical Receiver Front-End with a Monolithically Integrated Avalanche Photodetector in 0.25 μm SiGe BiCMOS Technology

J. S. Youn^{*}, M. J. Lee^{*}, K. Y. Park^{*}, H. Rücker^{**}, and W. Y. Choi^{*}

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Abstract

An 850-nm optical receiver front-end having a monolithically integrated avalanche photodetector is realized for optical interconnect applications with standard 0.25- μ m SiGe BiCMOS technology. Using fabricated optical receiver front-end, 9-Gb/s optical data are successfully transmitted with a bit-error ratio less than 10⁻⁹ at the incident optical power of -2 dBm.

1. Introduction

The data transmission capacity for many interconnect applications is rapidly increasing. With the conventional electrical interconnects, however, it is difficult to satisfy the requirement due to increasing channel loss, cross-talk noise and power consumption with the increasing transmission data rate. In order to solve these problems, optical interconnects have been actively investigated. In order to achieve low-cost optical interconnect solutions, various approaches have been studied. Among these, the silicon-based optical interconnects have emerged as a powerful solution due to their low fabrication cost and the possibility for monolithic integration with electronic circuits.

Various types of silicon photodetectors that can be realized with standard Si technology have been reported such as spatially modulated light (SML) [1], lateral PIN [2], N-well/P-substrate junction [3]. We have demonstrated silicon avalanche photodetectors (Si APDs) having much improved responsivity and detection bandwidth [4]. Furthermore, these silicon photodetectors have been monolithically integrated with CMOS [1-3], [5] and BiCMOS [6] electronic circuits and used for multi-gigabit optical data transmission demonstration.

In this paper, we report a monolithically integrated optical receiver front-end fabricated with standard 0.25- μ m SiGe BiCMOS technology. The optical receiver is composed of a Si APD and a transimpedance amplifier (TIA) having large feedback resistance (R_F) and capacitive degeneration technique. Without inductive peaking technique [7], our receiver has high gain-bandwidth (GBW) product of about 40 THz· Ω . Using the fabricated optical receiver front-end, we successfully demonstrate optical data transmission up to 9 Gb/s.



Fig. 1. Circuit diagram of the transimpedance amplifier having dc current rejection circuit and buffer with capacitive degeneration.

2. Monolithically Integrated Optical Receiver Front-End

Fig. 1 shows the circuit diagram of the TIA which is composed of shunt-feedback amplifiers, dc current rejection circuit, and buffer with capacitive degeneration. Its output signal is converted into fully differential signal by a single-to-differential amplifier and output buffer is designed for 50- Ω loads. Our receiver is fabricated in the 0.25- μ m SiGe BiCMOS technology SG25H3 of IHP. This technology provides SiGe HBTs with $f_T = 110$ GHz and $f_{max} = 180$ GHz [8]. The core chip size is about 480 μ m x 150 μ m and total power consumption of the electronic circuits excluding the output buffer is about 30 mW with the 2.5-V supply voltage.

The Si APD is realized by vertical P^+/N -well junction and its optical window is about 10 μ m x 10 μ m. The detailed structure and characteristic of Si APD are described in [4].

The shunt-feedback amplifier consists of two-stage amplifiers (common-emitter and emitter-follower configuration) and feedback resistance (R_F) of 5 k Ω . Although high feedback resistance reduces TIA bandwidth, it has advantages of lower input-referred noise and larger output signal. With SiGe HBTs having large GBW product, high-gain and high-speed characteristics can be simultaneously achieved. To keep stable dc operating points for the TIA circuit, the dc current of Si APD (I_{DC}) is subtracted from signal current of



Fig. 2. Measured photodetection frequency responses of the integrated optical receiver front-end.

Si APD (I_s). Then, with a replica shunt-feedback amplifier, an error amplifier, and a transistor (M_1), I_{DC} can be effectively eliminated. The replica shunt-feedback amplifier provides reference voltage at (-) node of the error amplifier and the transistor acts as a variable current source [9]. The buffer with capacitive degeneration generates zeroes in the TIA system response, which compensate poles due to Si APD and the shunt-feedback amplifier. In addition, by controlling the equivalent capacitance (C_{eq}) value from 100 fF to 400 fF, the zero location can be adjusted.

3. Measurement Results

Fig. 2 shows the measured photodetection frequency responses of the fabricated optical receiver front-end when the incident optical power (Popt) is -2 dBm and the applied reverse bias voltage (V_R) is 12.3 V, which is experimentally found to be optimal. The measured 3-dB bandwidth is about 2.45 GHz when $C_{eq.}$ is 100 fF. Its bandwidth is enhanced up to 5.6 GHz when $C_{eq.}$ is 400 fF. For optical data transmission measurement, 850 nm light from a laser diode is modulated with an electro-optic modulator using a 2^{31} -1 pseudo-random bit sequence. Modulated optical data are injected into the fabricated optical receiver using a lensed fiber. In order to satisfy input sensitivity requirement of the bit-error ratio (BER) tester, a 10-Gb/s commercial limiting amplifier is used. Fig. 3 shows the measured BER performance as a function of the incident optical power when 9-Gb/s optical data are transmitted. To minimize intersymbol interference, equivalent capacitance is set 400 fF for maximum receiver bandwidth. The inset of Fig. 3 shows the eye diagram of 9-Gb/s optical data with the BER less than 10^{-9} when the Popt of -2 dBm.

4. Summary

A high-gain and high-speed optical receiver front-end with an



Fig. 3. BER as a function of the incident optical power (P_{opt}) at data rate of 9 Gb/s. Inset shows the eye diagram of 9-Gb/s data rate at the P_{opt} of -2 dBm.

on-chip avalanche photodetector is demonstrated. It is fabricated with standard 0.25-µm SiGe BiCMOS technology without any process modification in a cost-effective manner. Using the fabricated optical receiver front-end, optical data up to 9 Gb/s are successfully demonstrated.

Acknowledgements

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